

Piezoconductivity of gated suspended graphene

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We investigate the conductivity of graphene sheet deformed over a gate. The effect of the deformation on the conductivity is twofold: The lattice distortion can be represented as pseudovector potential in the Dirac equation formalism, whereas the gate causes inhomogeneous density redistribution. We use the elasticity theory to find the profile of the graphene sheet and then evaluate the conductivity by means of the transfer matrix approach. We find that the two effects provide functionally different contributions to the conductivity. For small deformations and not too high residual stress the correction due to the charge redistribution dominates and leads to the enhancement of the conductivity. For stronger deformations, the effect of the lattice distortion becomes more important and eventually leads to the suppression of the conductivity. We consider homogeneous as well as local deformation. We also suggest that the effect of the charge redistribution can be best measured in a setup containing two gates, one fixing the overall charge density and another one deforming graphene locally.

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I. INTRODUCTION

Graphene is a novel material with highly unusual electron properties, related to the Dirac form of its energy spectrum at low energies, and demonstrated in many seminal experiments (for review see^{1,2}). Experiments on single-layer graphene have been performed on the flakes obtained by exfoliation as well as grown on a substrate.

Graphene also has excellent mechanical properties. Indeed, the elastic properties have been measured on suspended graphene flakes mechanically deposited over a hole by indentation in an atomic force microscope³⁻⁵; the results showed that graphene is incredibly stiff, with the breaking strength of the order of 40N/m, the Young modulus of 1 TPa, and possibility to be stretched elastically up to 20%. Bending properties have been determined experimentally for several-layer graphene flakes⁴ and are not yet available for a monolayer. Theoretically, these properties have been predicted from the calculations using the analytical form of the interatomic potential, and from molecular dynamic studies^{6,7}. Graphene is currently one of the most prospective candidates for high-frequency nanomechanical resonators^{8,9}, with the quality factor and eigenfrequency extracted from measurements to be $Q \approx 75$, $f_0 = 70.5$ MHz for a monolayer, and $Q \approx 120$, $f_0 = 42$ MHz for 15nm thick graphite. Quality factor further increases with decreasing temperature. An alternative method to investigate elastic properties of graphene is to put the film on a flexible substrate and deform the substrate^{10,11}. The strain influences optical phonon spectrum¹¹, which has been measured by Raman spectroscopy.

Recent experiments combine mechanical and electrical properties of graphene by measuring conductivity¹²⁻¹⁵ of suspended graphene flakes. This is a very promising direction since suspended graphene flakes exhibit much higher mobility than graphene on substrate due to much weaker disorder^{12,13}. Potentially electrons can produce

back-action on the resonator. Graphene resonators are expected to have high sensitivity to mass and prebuilt strain⁹, so that they can be used to ultra-sensitive mass detection.

Suspension of graphene flakes always leads to their deformation, which in turn affects the conduction properties of graphene. Deformation creates inhomogeneous elongation of the lattice constant^{16,17} which locally affects the electron spectrum of graphene. One way to look at the variations of the band structure of the strained graphene is to perform density functional calculations¹⁸. Alternatively, the variation of the lattice constant can be represented at the level of Dirac equation in the form of pseudomagnetic fields¹⁹. Ref. 17 pointed out that local shifts of the Fermi surface in suspended graphene in the vicinity of the Dirac point can block the conductivity — if the Fermi-surfaces at different parts of the flake do not overlap, the conduction is tunnel rather than metallic. Effects of disorder due to charged impurities and midgap states, optical and acoustic phonons were taken into account for calculating conductivity of gated graphene in²⁰. For strong enough deformation, graphene quasiparticles can become localized²¹.

In experiments, graphene flakes are typically suspended over a back-gate. This gate redistributes the electron density in the flake due to the spatial variation of the capacitance. The regions in the center of the suspended part of the flake have higher electron density than the regions near the clamping edges, as the central part is closer to the gate. This density redistribution affects the transmission coefficients through the entire flake. The corresponding effect on the piezoresistivity in ballistic regime is of the first order in the maximum deformation of the flake in the transverse direction, and it increases the conductivity. This has to be contrasted with the effect of the pseudomagnetic fields which suppress the conductivity. The contribution from pseudovector potential depends on the strain¹⁷ over the flake and is of the sec-

ond order in the maximum deformation. Thus, this contribution is expected to be weaker than effect from the charge redistribution. We will show however that this effect can be important for graphene under high enough residual stress. Inhomogeneous deformation of graphene yields the corrections to the conductivity which are of the fourth order in the maximum deformation, which is even smaller.

In this Article, we calculate the effect of the gate-induced density redistribution on the conductivity of the graphene flake. We find that, indeed, for high residual stress the correction resulting from the pseudovector potential is important, and the correction to the conductivity is negative. We mostly focus on the regime of low residual stress and show that the correction from the charge redistribution becomes the most important.

Experimentally, influence of deformation on the conductivity would be difficult to observe on a suspended graphene flake with one gate since the main effect of the gate is the global shift of the density rather than its redistribution. To separate density redistribution and elastic deformation, one needs to employ two gates. For instance, one can use the configuration with a large bottom gate and a narrow top gate. The bottom gate deforms the graphene flake and determines the maximum transverse deformation ξ_{max} . When voltage is switched on the narrow top gate it does not influence much of deformation of the flake depleting the charge density below the top gate. Since the region under the top gate has the lowest density it determines the conductivity of the whole flake. If this region is brought to the Dirac point, the correction to conductivity is determined only by the deformation of graphene¹⁷ and is proportional to $(\xi_{max}(V_g)/L)^2$, with V_g and L being the voltage applied to the bottom gate and the length of the strip under the top gate. However, for higher voltages the charge redistribution is more important, and the correction to conductivity is proportional to $\xi_{max}(V_g)/d$, d being the distance to the bottom gate. Instead of the top gate, one can use an AFM tip.

The paper is organized as follows. In Section II we derive equations for the deformation of suspended graphene from general theory of elasticity. We consider two situations — graphene deformed homogeneously by a gate and graphene deformed locally by an AFM tip. The capacitance between the gate and suspended graphene varies due to deformation of the flake. We calculate the density redistribution over the flake taking into account the shape of the flake. In Section III, we use these results to evaluate correction to the conductivity. We use the perturbation theory to calculate the transmission eigenvalues, and the correction to the conductivity is obtained using the Landauer formula. This correction can be big for sufficiently strong deformations of the flake which can be produced by an AFM tip. In Section IV we discuss the results and the regimes not considered in this Article.

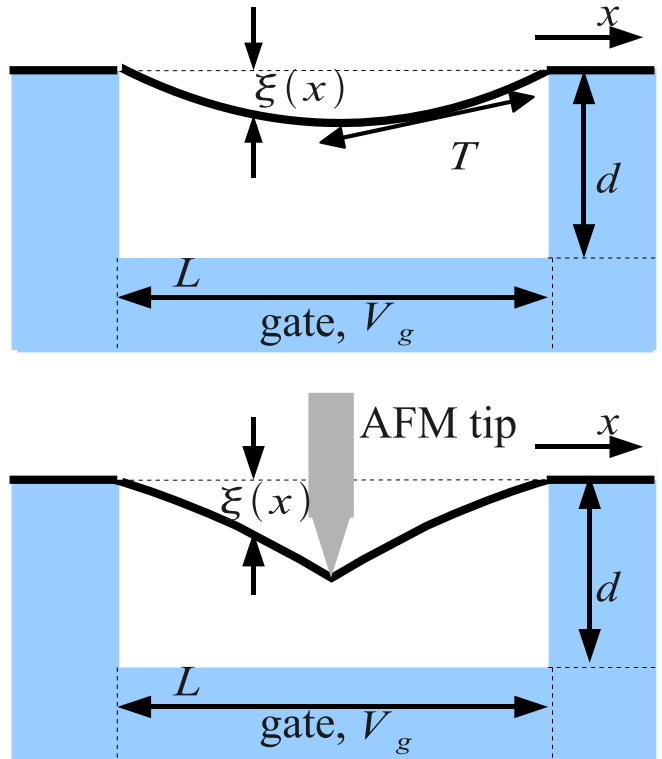


FIG. 1: Side view of a deformed graphene flake suspended over a gate. The deformation is caused only by the interaction with a gate (top) or by the gate and an AFM-tip (bottom).

II. DEFORMATION OF THE GRAPHENE SHEET

In this Section, we calculate the profile of the graphene sheet formed by electrostatic forces induced by the gates. For this purpose, we decompose the total energy of the flake as the sum of electrostatic and elastic energies. We consider a graphene flake of the length L (direction x) and the width W (direction y). For simplicity, we assume $W \gg L$. An undeformed sheet occupies a part of the plane $z = 0$; the electrostatically induced deflection is $\xi(x, y)$. Below we only consider small deformations so that we can stay within the limits of linear theory of elasticity (Hooke's law). At stronger deformations, as expected from the general theory²³ and also confirmed by theoretical modeling²⁴ and by experiments⁸ on graphene, non-linear terms become important. However, there is a considerable parameter range, with the displacements up to 50 nm, where the linear regime is still valid. We discuss the terms which go beyond Hooke's law²⁴ in Section IV.

For electrostatic energy, similarly to Ref. 25, we model the system as a capacitor between the flake and the gate, with the distributed capacitance C_g dependent on the

profile of the flake,

$$C_g = \int c[\xi(x, y)] dx dy. \quad (2.1)$$

Electrostatic coupling to the leads is modelled via contact capacitances C_L , C_R and resistances R_L , R_R , see Fig (1). The total electrostatic energy of the system carrying the charge Q is

$$F_{electr} = -\frac{Q^2}{2C_0} + \frac{Q}{C_0}(C_L V_L + C_g V_g) - \frac{C_L C_g V_L V_g}{2C_0} + \frac{C_L V_L^2 (C_0 - C_L)}{2C_0} + \frac{C_g V_g^2 (C_0 - C_g)}{2C_0},$$

with $C_0 = C_L + C_R + C_g$.

From now on, we assume that the contacts are ideal, $C_L = C_R = 0$, and thus the electrostatic energy is

$$F_{electr} = -\frac{Q^2}{2C_g} + Q V_g. \quad (2.2)$$

The effect of non-ideal contacts is discussed in Section IV.

A. Elastic energy

We evaluate the elastic energy in the thin-plate approximation. The elastic energy consists of the bending contribution $F_1(\xi(x, y))$ and the stretching contribution $F_2(u_{\alpha\beta}(x, y))$, where $u_{\alpha\beta}(x, y)$ is the deformation tensor, and α and β denote the coordinates in the plane of the sheet (x and y). In the linear regime, the bending contribution is less important than the stretching one, however, we consider both contributions for completeness. Explicitly, we have²³

$$F_1(\xi) = \frac{D}{2} \int \int dx dy \left(\frac{\partial^2 \xi}{\partial x^2} + \frac{\partial^2 \xi}{\partial y^2} \right)^2 + \int \int dx dy (1 - \sigma^2) \left[\left(\frac{\partial^2 \xi}{\partial x \partial y} \right)^2 - \frac{\partial^2 \xi}{\partial x^2} \frac{\partial^2 \xi}{\partial y^2} \right] \quad (2.3)$$

and

$$F_2(u_{\alpha\beta}) = h_0 \frac{u_{\alpha\beta} \sigma_{\alpha\beta}}{2}. \quad (2.4)$$

Here $D = Eh_0^3/(12(1 - \sigma^2))$ is the bending rigidity, E is the Young modulus, σ is the Poisson ratio, h_0 is the thickness of the plate (graphene flake), and $\sigma_{\alpha\beta}$ is the stress tensor.

In addition, if a local force (for instance, an AFM tip) acts on the graphene flake, it is best represented by external pressure $P_{ext}(x, y)$. The work of this external pressure to deform the flake by $\delta\xi(x, y)$ is $F_3 = \int P_{ext} \delta\xi(x, y) df$, where df is the surface element.

The profile of the sheet is determined by minimizing its total energy. Performing the variation, we find the equation describing the shape of the flake,

$$D\Delta^2 \xi - \frac{\partial}{\partial x_\beta} (h_0 \sigma_{\alpha\beta} \frac{\partial \xi}{\partial x_\alpha}) = P_{el}(x, y) + P_{ext}(x, y), \quad (2.5)$$

$$\frac{\partial \sigma_{\alpha\beta}}{\partial x_\beta} = 0, \quad (2.6)$$

with $P_{el}(x, y)$ being the electrostatic pressure on the plate, induced by the variation of electrostatic energy (2.2). For ideal contacts, $P_{el}(x, y) = n^2(x, y)/2\epsilon_0$. Here $n(x, y)$ is the electron density. Eq. (2.5) is the most general equation for $\xi(x, y)$ in the linear approximation of theory elasticity. For an infinitely wide graphene flake, $W \gg L$, the deformation in the y direction is homogeneous.

At sufficiently small deformations, the tension along the sheet is constant over the sheet (2.6), $h_0 \sigma_{\alpha\beta}^0 = T \delta_{\alpha\beta}$. The tension T is the sum of two contributions:

$$T = T_0 + T_H, \quad T_H = \frac{E h_0}{1 - \sigma^2} \Delta L / L \quad (2.7)$$

The first one, T_0 , is the residual stress which results from the fabrication process or is induced by the ripple formation^{3,4}. The second contribution, T_H , is an internal force due to the relative elongation $\Delta L/L$ (Hooke's law). If we take this term into account, we can go beyond the thin-plate approximation and consider deformations bigger than the thickness of the graphene layer.

In the two following Subsections, we solve the above equations for two specific situations: homogeneous external force (which can be produced by a bulk bottom gate), and local force (produced for example by an AFM tip).

B. Homogeneous force: Deformation by a bottom gate

Applying a voltage on a bottom gate is a standard way to vary electron density in graphene. If the suspended graphene flake is charged, it is subject to a mechanical force proportional to the charge density. If the area of the gate is much larger than the area of the flake, the electron density induced by the gate is constant almost everywhere, $n = Q/WL$, except for the clamping points of the flake, where it is determined not only by the solution of the Poisson equation (providing singularities at the capacitor edges), but also by the metallic leads to which the flake is clamped. Indeed, experimental evidence for this charge inhomogeneity exist and can be accessed by asymmetry of the Dirac peak in conductivity⁴⁰. However, these density inhomogeneities at the clamping areas very little affect the deformation, since the displacement vanishes at the edges of the flake. Therefore we can approximate the effect of the gate by homogeneous electrostatic pressure over the flake, $P = \epsilon_0 V_g^2 / 2d^2$, V_g and d

being the gate voltage and the distance to the gate. The profile of the graphene sheet is found from the equation

$$D \frac{\partial^4 \xi}{\partial x^4} - T \frac{\partial^2 \xi}{\partial x^2} = P, \quad (2.8)$$

where the stress T is constant over the sheet (2.7) and the deformation-dependent contribution to it depending has to be found self-consistently,

$$T_H = \frac{Eh_0}{2(1-\sigma^2)} \int_0^L \xi'^2(x) dx \quad (2.9)$$

(the case for inhomogeneous T_H derived in Ref. 24 is discussed in Section IV and does not induce significant difference in results). For the boundary condition corresponding to the clamping the sheet, $\xi(0) = \xi(L) = \xi'(0) = \xi'(L) = 0$, the profile is

$$\xi(x) = \frac{PL}{2T\mu} \left[\frac{\sinh \mu L}{\cosh \mu L - 1} (\cosh \mu x - 1) - \sinh \mu x + \mu x - \frac{\mu x^2}{L} \right], \quad \mu = \sqrt{\frac{T}{D}}. \quad (2.10)$$

The profile (2.10) is parabolic in the middle of the strip (as noted in Ref. 17). As we show below, in graphene the dimensionless parameter μL assumes large values. In this case, the profile can be simplified, and near the middle of the strip has the form

$$\xi(x) = \frac{PL}{2T} \left(x - \frac{x^2}{L} \right). \quad (2.11)$$

Close to the edges, the profile becomes $\xi(x) = P\mu L x^2/4T$. Substituting this shape into Eqs. (2.3) and (2.4), we find the values of the parameters F_1 and F_2 ,

$$F_1 = \frac{P^2 L W}{16 T \mu^2 (-8 + \mu L)}, \quad (2.12)$$

and

$$F_2 = \frac{T^2 W L (1 - \sigma^2)}{E h_0}. \quad (2.13)$$

The maximum vertical displacement obeys the equation

$$\xi_{max} = \frac{PL^2}{8(T_0 + 8Eh_0\xi_{max}^2/(3(1-\sigma^2)L^2))}. \quad (2.14)$$

The deformation of the sheet leads to the redistribution of the electron density, which in the Thomas-Fermi approximation is $n(x) = V_g \epsilon_0 / (d - \xi(x))$. In its turn, the density redistribution affects the profile of the sheet, and needs, in principle, to be calculated self-consistently. However, as soon as the displacement ξ_{max} is much smaller than the distance to the gate, the later effect is insignificant (of the order of ξ_{max}/d), and we will use the shape (2.10) not modified by the density redistribution.

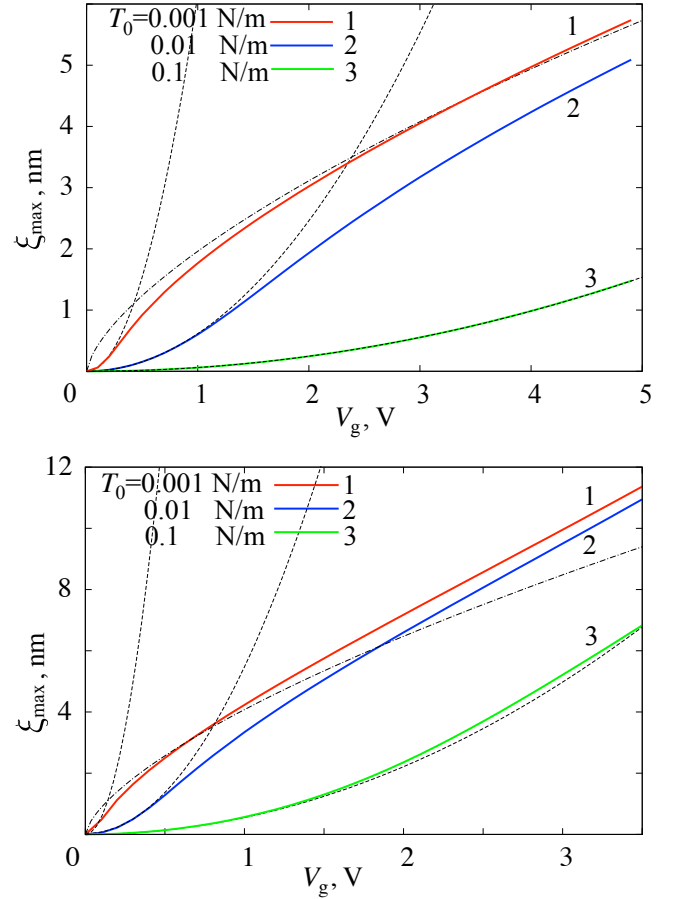


FIG. 2: Dependence of the maximum deviation on the gate voltage, $\xi_{max}(V_g)$. The solid curves represent the self-consistent solution of nonlinear coupled equations for the deformation of the flake and the charge induced by the gate, Eqs. (2.14) and (2.16). The distance to the gate is $d = 300$ nm (top panel) and $d = 100$ nm (bottom panel). Other parameters of the graphene flake, length $L = 1 \mu\text{m}$, Young's modulus $E = 1$ TPa, Poisson ratio $\sigma = 0.15$, and the thickness of the flake $h_0 = 0.34$ nm, are chosen in order to model real experimental data. The results are given for the different values of the residual stress: the curve 1 is for $T_0 = 0.001$ N/m, 2 is for $T_0 = 0.01$ N/m, 3 is for $T_0 = 0.1$ N/m. For each value of the residual stress, the asymptotic curves at low gate voltages (2.17) are shown as dashed lines, the curve 3 for high residual stress coincide perfectly with its asymptote. The asymptotic curves for low residual stress, Eq. (2.19), are shown by dashed-dotted lines. The correspondence between the solution of equations and asymptotics for low residual stress is not perfect. The reason is that the asymptotics are calculated for the linear charge-voltage dependence, and $n(V_g)$ is non-linear according to Eq. (2.16) for sufficiently high gate voltages on the flake.

The charge over the graphene flake is determined from minimization of the total energy of the system with re-

spect to electron density n ,

$$-V_g + \frac{nd}{\epsilon_0} \left[1 - \frac{8}{3} \frac{\xi_{max}}{d} + \left(1 + \frac{1}{2} \right) \frac{\xi_{max}}{d\mu L} + \frac{1}{3} \frac{\xi_{max}}{d} \right] = 0, \quad (2.15)$$

where the maximum deformation of the sheet in the middle, ξ_{max} (2.14), and depends on charge density. The second term in the brackets and 1 from the third term come from electrostatic energy and originate from the redistribution of the charge density due to variation of the distance between parts of deformed graphene and the gate. The rest (1/2) of the third term comes from bending energy. The fourth term takes into account dependence of the stretching force T over the flake on the charge density via the deflection (Eq. (2.9)). Calculations are made under the assumption $\mu L \gg 1$, which is realistic for available experiments. Simplifying Eq. (2.15), we obtain

$$-V_g + \frac{nd}{\epsilon_0} \left(1 - \frac{7}{3} \frac{\xi_{max}}{d} + \frac{3}{2} \frac{\xi_{max}}{d\mu L} \right) = 0 \quad (2.16)$$

At low gate voltages, Eq. (2.16) yields the linear gate voltage dependence of the electron density, $n_0 \equiv V_g \epsilon_0 / d$. There is non-linear deviation from this dependence at higher gate voltages and at rather low initial strain T_0 .

The maximum deformation can be expressed analytically in two limiting cases. First, if the residual stress T_0 is stronger than the induced stress T_H , it mostly accounts for the deformation of the sheet,

$$T_H = \frac{Eh_0 P^2 L^2}{24(1-\sigma^2)T_0^2} \ll T_0, \quad \left(\frac{Eh_0 P^2 L^2}{24(1-\sigma^2)} \right)^{1/3} \ll T_0,$$

$$\xi_{max} = \frac{\epsilon_0 V_g^2 L^2}{16d^2 T_0}, \quad (2.17)$$

$$\frac{n - n_0}{n_0} = \frac{7}{3} \frac{\xi_{max}}{d} \left(1 - \frac{72}{7\sqrt{T_0/DL}} \right). \quad (2.18)$$

In the case of low residual stress, one obtains

$$T_0 \ll T_H = \frac{1}{2} \left(\frac{Eh_0 P^2 L^2}{3(1-\sigma^2)} \right)^{1/3},$$

$$\xi_{max} = \frac{1}{4} \left(\frac{3V_g^2 \epsilon_0 (1-\sigma^2) L^4}{2d^2 Eh_0} \right)^{1/3}, \quad (2.19)$$

$$\frac{n - n_0}{n_0} = \frac{7}{3} \frac{\xi_{max}}{d} - 12 \sqrt{\frac{3D(1-\sigma^2)}{2Eh_0}}. \quad (2.20)$$

The maximum deviation ξ_{max} , obtained from the numerical solution of coupled nonlinear equations Eqs. (2.14), (2.16), as well as asymptotic expressions (2.17) and (2.19), are shown in Fig. 2 for different values of initial stress T_0 ²⁶. According to Eqs. (2.18) and (2.20), the nonlinear part of the charge induced on the graphene flake follows the dependence $\xi_{max}(V)/d$. Consequently, we encounter several regimes for the deformation,

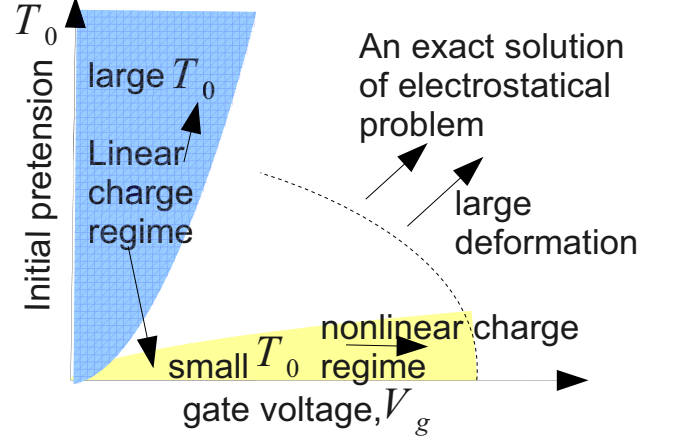


FIG. 3: Regimes of the deformation of suspended graphene. For large residual stress T_0 the asymptotics Eq. (2.17) are valid, and the charge on the flake follows the gate voltage linearly. For small T_0 the asymptotics Eq. (2.19) are valid, the charge is linear with the gate voltage at low gate voltages and starts to follow non-linear dependence with increasing voltage. At high gate voltages, when the deformation of the flake is bigger than $\xi_{max}/d \sim 0.1$, one needs to solve self-consistently the electrostatic problem and the problem of elasticity, analytical results for this region are not available.

- at large T_0 the charge–voltage dependence is linear for realistic parameters because the maximum deformation is not too large for realistic characteristics of graphene flake. It is shown in Fig. 2 for $T_0 = 0.1$ N/m that the maximum deformation is in a good agreement with Eq. (2.17);
- at small T_0 and low gate voltages V_g the charge–voltage dependence can be in linear regime, and the maximum deformation follows Eq. (2.19). We illustrate this for the flake with the parameters $T_0 = 0.001$ N/m and distance to the gate $d = 300$ nm (See. Fig. 2, top), where the solutions of coupled electrostatic and elastic equations, Eq. (2.14), (2.16), follow asymptotic expression Eq. (2.19). The charge redistribution does not need to be taken into account;
- at small T_0 and large V_g the system is in the non-linear charge regime. This situation can be realized for small distances to the gate when the coupling of the graphene sheet to the gate is large, so that it is possible to create large deformations using low gate voltages. For example, at $d = 100$ nm the non-linear charge regime influences the deformation already at voltage $V_g = 2$ V, at the bottom plot Fig. 2 we can see the intersection of the asymptotical curve (2.19) and the actual solution of Eqs. (2.14), (2.16).

The schematic representation of these regimes is shown

in Fig. 3.

C. Local force: Deformation by an AFM tip

Next, we consider a concentrated force acting on graphene. This force can be provided, for example, by an AFM tip. The effect of the tip is modeled by strong pressure exerted on a narrow area of the width $l \ll L$. We assume that the problem is still homogeneous in the y -direction, what simplifies the calculations enormously. Inclusion of a pressure action in a narrow circle, which is experimentally relevant for an AFM tip, is not expected to bring qualitatively new features. We consider pressure $P(x) = P_2, 0 < x < L/2 - l/2, L/2 + l/2 < x < L$ and $P(x) = P_1, L/2 - l/2 < x < L/2 + l/2$. Here P_2 is the local pressure, and $P_1 \ll P_2$ can describe homogenous pressure due to electrostatics.

The maximum displacement of the flake (realized at the central point) is easy to write down for $\mu L \gg 1$ and $l \ll L$:

$$\xi_{max} = \frac{P_1 ((\mu L/2)^2 e^{\mu l/2} - 2e^{-\mu l})}{2\mu^2 T} + \frac{P_2 (e^{-\mu l} + e^{\mu l} \mu^2 l L/4)}{\mu^2 T}. \quad (2.21)$$

For $P_1 \ll P_2$ and $1 \ll e^{\mu l/2} L \mu l \mu/4$ we obtain

$$\xi_{max} = \frac{P_2 l L}{4T}. \quad (2.22)$$

The profile of the graphene sheet in this approximation becomes

$$\xi(x) = \frac{2\xi_{max}}{L} |x - L/2|. \quad (2.23)$$

In the limits of weak and strong residual stress the deformation is determined by

$$T_H = \frac{Eh_0}{8(1-\sigma^2)} \left(\frac{P_2 l}{T_0} \right)^2 \ll T_0, \left(\frac{Eh_0}{8(1-\sigma^2)} P_2^2 l^2 \right)^{1/3} \ll T_0,$$

$$\xi_{max} = \frac{P_2 l L}{4T_0}; \quad (2.24)$$

and

$$T_0 \ll T_H = \frac{1}{2} \left(\frac{Eh_0 P_2^2 l^2}{1-\sigma^2} \right)^{1/3}, T_0 \ll \frac{1}{2} \left(\frac{Eh_0 P_2^2 l^2}{1-\sigma^2} \right)^{1/3},$$

$$\xi_{max} = L \left(\frac{P_2 l (1-\sigma^2)}{8Eh_0} \right)^{1/3}. \quad (2.25)$$

The dependence of the maximum deformation on the applied external local force is shown in Fig. 4. The deformation produced by this force is much bigger than the deformation caused by electrostatic pressure of the gate. The electrostatic problem for this case can be solved separately from the problem of elasticity.

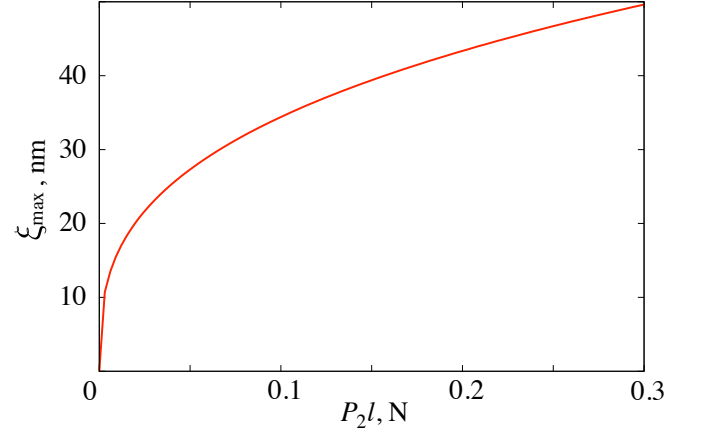


FIG. 4: Dependence of the maximum deformation ξ_{max} on the applied force $P_2 l$ for the case of the point force in the middle of the graphene sheet. Only the curve for $T_0 = 0$ is shown, since the residual stress is not important for this case: The strain created by deformation becomes large (more than 0.1 N/m) already at moderate deformations in the middle, $\xi_{max} \sim 10$ nm. Other parameters of the flake are²⁶.

III. PIEZOCONDUCTIVITY OF GRAPHENE FLAKE

It was shown experimentally¹³ that suspended graphene flakes are described with good precision as purely ballistic. Theoretically, conductance is determined by Landauer formula²⁷

$$\sigma = 4e^2/h \sum_{n=0}^{N-1} T_n, \quad (3.1)$$

where T_n is the transmission eigenvalue in the transport channel n , and the factor $4e^2/h$ is conductivity of a single transport channel which takes into account valley and spin degeneracy. The number of open transport channels $N = Wk_F/\pi$ is proportional to the Fermi momentum $k_F = (\pi n/e)^{1/2}$, and thus the conductivity is proportional to the square root of the electron density n , $\sigma \propto \sqrt{n}$.

The conductivity of graphene flake suspended over a gate can deviate from this dependence. To start with, due to electrostatic interaction with the gate, the density becomes inhomogeneous²⁸. In particular, Poisson equation leads to the square root divergence of the electron density at the clamping points, as in any capacitor (see e.g. Ref. 29). To treat this divergence properly, one has to take into account electrostatic interaction with the contacts near the edge of the graphene strip, which modifies significantly the electron density near the edge, removing the divergence. However, the effect of this inhomogeneous density close to the contacts does not affect the piezoconductivity of the flake, since the deformation close to the clamping points is very weak, and thus it can be included into the contact resistance at the clamping points.

We now turn to the effects of the deformation on the conductivity. Deformation of graphene can change the conductivity by inducing changes in the band structure (which results in pseudo-magnetic fields) as well as by changing the electron density over the flake. We consider both these mechanisms and will show that typically the effect of the density redistribution dominates.

Electrons in graphene obey Dirac equation. Deformation of the flake influences on the Dirac equation in three ways — it shifts the K-points by a certain amount $\delta k/k_F$ (pseudomagnetic field), renormalizes the Fermi velocity by $\delta v_F/v_F$, and induces the variation of the electron density on the flake $\delta n/n$. The deformation correction to the conductivity is thus a function of these three dimensionless parameters.

The pseudomagnetic field, produced by the shift of the K-point, is caused by stretching and bending. The shift of the K-point due to stretching generates the vector potential^{17,19}

$$A_y^{str} = \frac{C\tilde{\beta}}{a}(u_{xx} - u_{yy}), \quad A_x^{str} = -2\frac{C\tilde{\beta}}{a}u_{xy}, \quad (3.2)$$

where C is the order of 1, and $\tilde{\beta} = -\partial \log(t)/\partial \log(a)$, t and a being the overlap integral in the tight-binding model and the lattice parameter, respectively. For $L \ll W$ one has $u_{xy} = 0$, and hence $A_x^{str} = 0$. The deformation is homogeneous within the limits of applicability of Hooke's law, and thus $u_{xx} = \text{const}$ and $A_y^{str} = \text{const}$. This means that there is no pseudomagnetic field over the graphene flake. The pseudomagnetic field only appears in the region where the flake goes from the substrate to the suspended state¹⁷ and, as noted above, its effect to the piezoconductivity is small, of the second order in ξ_{max}/L ,

$$\frac{d\sigma_K}{\sigma} = \frac{A_y^{str}}{k_F}, \quad (3.3)$$

where the deformation on the edges has been estimated as $u_{xx} = \xi_{max}^2/L^2 + T_0(1 - \sigma^2)/Eh_0$, and $k_F = \sqrt{\pi\epsilon_0 V_g/d\epsilon}$. Taking into account the value of $C\tilde{\beta}/a$ ³⁰, we obtain

$$\frac{\delta\sigma_K}{\sigma} = 205 \sqrt{\frac{d[\mu\text{m}]}{V_g[\text{V}]}} \left(\frac{\xi_{max}^2}{L^2} + \frac{T_0(1 - \sigma^2)}{Eh_0} \right). \quad (3.4)$$

Note the contribution from two terms induced by deformation stress and residual stress, as well as multiplication with the big prefactor 205.

The underlying physical picture for the model of Ref. 17 is that the graphene flake is "glued" to the walls at the suspension point. Whereas this has been realized in some experiments³, it describes the situation when the residual strain T_0 is of the same order or higher than the strain induced by the gate voltage. The residual strain results from the fabrication process and is most likely to be created by impurities in the substrate. It can be made low on purpose since the strain is reduced after annealing⁹. In the opposite situation, when the residual stress

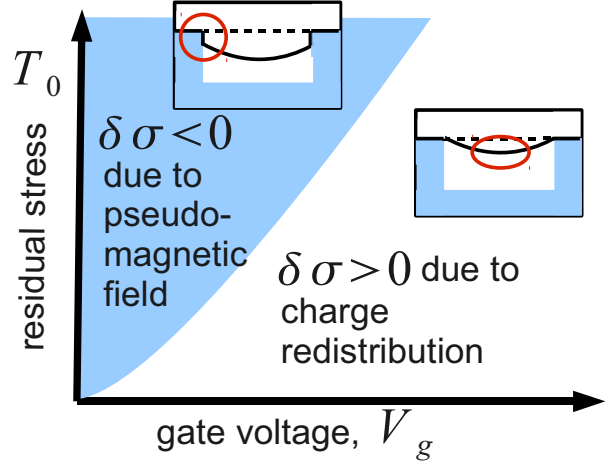


FIG. 5: Schematic behavior of piezoconductivity. For low residual stress T_0 the correction is mainly due to the charge redistribution and has positive sign. For high residual stress the correction is negative.

is not significant, the pseudomagnetic field is inhomogeneous and distributed over the whole suspension area.

The pseudomagnetic field is also inhomogeneous if one considers the bending contribution. Bending leads to the inhomogeneous modification of the overlap of the orbitals, and the resulting pseudovector potential has the form³¹

$$A_y^{bend} = \frac{t_{bend}}{a} \left(\frac{\theta^2(a, x)}{2} - \frac{\theta^2(\frac{a}{2}, x)}{2} \right), \quad (3.5)$$

$\theta(a, x)$ being the angle between normal vectors to the graphene surface at the points x and $x + a$, and the constant³² $t_{bend} = 3.21$ ³³. The shape dependence of $\theta(a, x)$ has the form

$$\theta^2(a, x) = a^2 \left(\frac{\partial^2 \xi}{\partial x^2} \right)^2 \left(1 + \left(\frac{\partial \xi}{\partial x} \right)^2 \right)^{-1}.$$

This yields $A_y^{bend} \approx (3t_{bend}/8a)(\xi_{max}a/L^2)^2$. Hence the contribution from bending is approximately $(a/L)^2$ times smaller than from stretching without residual stress, and is thus negligibly small, even though the resulting magnetic field is not homogeneous.

The easiest way to estimate inhomogeneous stretching of graphene is to take Hooke's law in the local form, $T_H(x) = Eh_0 u_{xx}(x)$. Since the maximum relative deformation can be estimated as $u_{xx} = \xi_{max}^2/L^2$, naively, the correction from non-homogeneous stretching is of the same order as the one from delta-functional pseudomagnetic field at the clamping edges. We show below, however, that the correction from non-uniform stretching is of the order of ξ_{max}^4/L^4 , but still due to large prefactor it can reduce the conductivity at low gate voltages.

Another effect induced by the deformation is the renormalization of the Fermi velocity. The renormalized

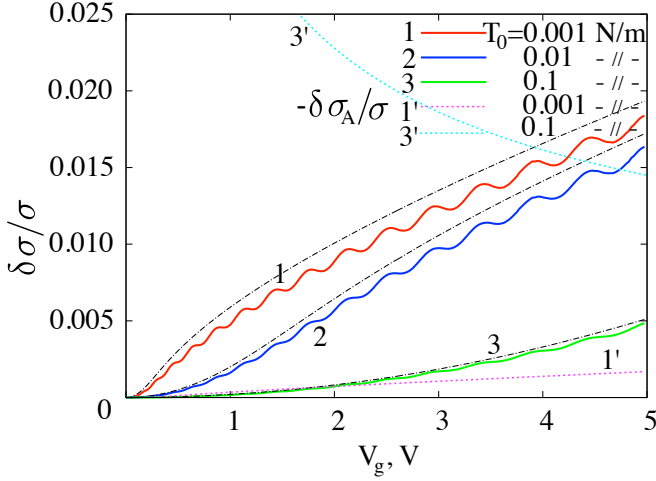


FIG. 6: The correction to conductivity. Parameters of the flake are the same as for Fig. 2 (top). Asymptotic expressions for the high gate voltage are shown by the dashed-dotted lines. Additionally, the correction due to the delta-functional pseudomagnetic field at the suspension regions¹⁷, Eq. (3.4), is shown (with the opposite sign).

value of the velocity can be derived from the tight-binding model. Assuming that the graphene sheet is only deformed in the x -direction, we find that the x -component of the Fermi velocity is unchanged whereas the y -component is renormalized,

$$v_{Fy} = v_F(1 - C\tilde{\beta}u_{xx}), \quad (3.6)$$

so that approximately $v_{Fy} \approx v_F(1 - \xi_{max}^2/L^2)$. The effect of the renormalization on the conductivity is not significant and has the order of magnitude ξ_{max}^2/L^2 . Note that this is the same dependence on ξ_{max}/L as for pseudomagnetic fields, however, it is not enhanced by a big prefactor.

The influence on conductivity of such change in fermi-velocity is not significant. This influence can be in principle measured experimentally as the conductivity variation at the Dirac point, similarly to how we explain below in Subsection III B.

A. Correction to conductivity due to the charge redistribution

Redistribution of electric charge due to interactions with the gate is found from the assumption that the potential along the graphene sheet is constant, $U(x) = \delta Q(x)/\delta C(x) = \text{const}$, where $\delta C(x)$ is the capacitance of the element of the length δx of graphene, $\delta C(x) = W\delta x/4\pi(d - \xi(x))$, and $\delta Q(x) = n(x)W\delta x$ is the charge of this element. In the first order approximation, this gives $\delta n(x)/n_0 = \xi(x)/d$.

The conductivity of graphene is proportional to charge density n , and thus the contribution to conductivity due to charge redistribution is expected to be linear in

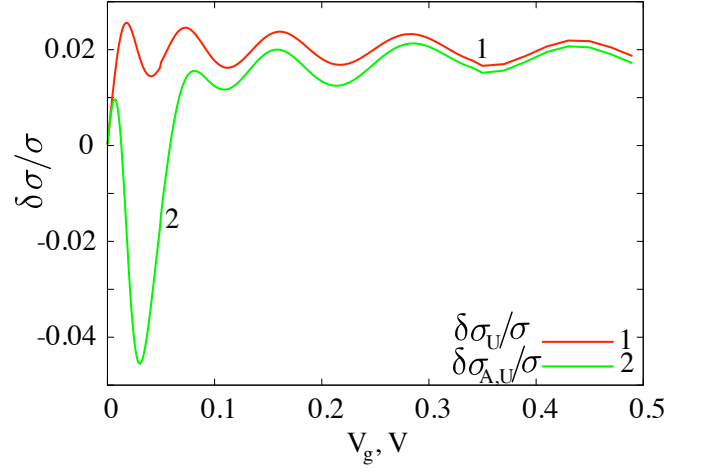


FIG. 7: Dependence of the piezocorrection to conductivity on the gate voltage for fixed deformation, obtained by solving the Dirac equation by exact transfer matrix method. Here, $\delta\sigma_U$, the curve marked 1, is the correction with only charge redistribution taken into account, and $\delta\sigma_{A,U}$, the curve 2, encompasses both contributions, the one due to non-uniform tension and the one due to charge redistribution. At low gate voltages the correction $\delta\sigma_{A,U}$ is mostly caused by pseudo-magnetic field and is negative, for higher gate voltages it changes sign and approaches to $\delta\sigma_U$. Parameters of the graphene flake are²⁶.

the maximum deviation from the homogeneous density, δn_{max} . Thus, the correction to conductivity is expected to be $\delta\sigma/\sigma \sim \xi_{max}/d$. Before starting the calculation of the correction to conductivity, we estimate the range where this correction of the order of ξ_{max}/d is more important than the correction due to pseudovector potential which we considered above, Fig. 5,

$$T_0[\text{N/m}] < 10^{-3} \frac{L}{d} \sqrt{\frac{V_g^{5/2}[\text{V}]}{d^{3/2}[\mu\text{m}]}}, \quad (3.7)$$

As noticed in Ref. 17 the pseudovector potential at low gate voltages blocks conductivity, this is seen from Eq. (3.4). For large deformation the expressions (2.19) are valid, residual stress is not important any more, and thus the gate voltage should be large enough to see the decrease of conductivity,

$$V_g[\text{V}] > 2.8 \frac{L^4}{d^4} \frac{1}{d[\mu\text{m}]}. \quad (3.8)$$

This deformation is so strong that it can not be reached in practice.

For the deformation with AFM the residual stress is not important and at deviations

$$\xi_{max}[\text{nm}] > 2.5 \frac{L^2[\mu\text{m}]}{d[\mu\text{m}]} \sqrt{\frac{V_g[\text{V}]}{d[\mu\text{m}]}} \quad (3.9)$$

correction to pseudovector potential starts to suppress the conductivity.

To calculate the correction due to the charge redistribution, we notice that the density variation is translated into the correction for conductivity via the variation of the transmission probabilities T_n , which are the eigenvalues of the matrix $\hat{t}^\dagger \hat{t}$, \hat{t} being the transmission matrix of the graphene sheet. The transmission eigenvalues t_q are determined in Appendix by the transfer matrix method. The correction to the conductivity is linear in the density shift δn , and consequently in the maximum deformation ξ_{max} (as is shown above from simple qualitative considerations). It has the form (see Appendix)

$$\delta\sigma_U = \sum_q 4|t_q|^2 \frac{q^2 k_F^2}{k^3} \sin kL \times \int_0^L dx \frac{\xi(x)}{d} \sin k(L-x) \sin kx, \quad (3.10)$$

where $|t_q|^2 = (\cos^2 kL + k_F^2 \sin^2 kL/k^2)^{-1}$ is the transmission probability for the mode labeled by the transverse momentum $q = 2\pi n/W$, n being an integer number, and k is a wave number in the direction along the strip, so that $k_F^2 = k^2 + q^2$.

To carry out more detailed analysis, we consider specific deformation setups discussed in Section II — homogeneous and local deformation.

Eq. (3.10) can be analyzed analytically for small and large values of the parameter $k_F L$, which characterizes the charge density over the flake. The correction to conductivity for the homogeneous deformation (bottom gate) has the following asymptotic behavior for small and large values of $k_F L$ (for more details, see Appendix),

$$\frac{\delta\sigma}{\sigma} = \begin{cases} \xi_{max}/2d, & 1 \ll k_F L; \\ 0.021 \xi_{max} (k_F L)^2/d, & k_F L \ll 1. \end{cases} \quad (3.11)$$

Taking into account the functional dependence of the maximum deviation for small and large initial stress T_0 , Eqs. (2.19) and (2.17), we get the asymptotic dependence of the correction to conductivity on the gate voltage, for $T_H \ll T_0$:

$$\frac{\delta\sigma(V)}{\sigma(V)} \sim \begin{cases} L^2 V^2 / T_0 d^3, & 1 \ll k_F L; \\ L^4 V^3 / T_0 d^4, & k_F L \ll 1, \end{cases} \quad (3.12)$$

and for $T_0 \ll T_H$:

$$\frac{\delta\sigma(V)}{\sigma(V)} \sim \begin{cases} L^{4/3} V^{2/3} / d^{5/3}, & 1 \ll k_F L; \\ (V L^2 / d^2)^{5/3}, & k_F L \ll 1. \end{cases} \quad (3.13)$$

Fig. 6 shows the exact result of summation over modes Eq. (3.10). At both high ($k_F L \gg 1$) and low ($k_F L \ll 1$) gate voltages, the correction follows the asymptotic behavior both for weak and strong residual stress T_0 , Eqs. (3.13) and (3.12). On the same plot we compare the correction we found with the correction due to pseudomagnetic fields at the edges¹⁷. The latter one has a different sign (conductivity decreases with the stress).

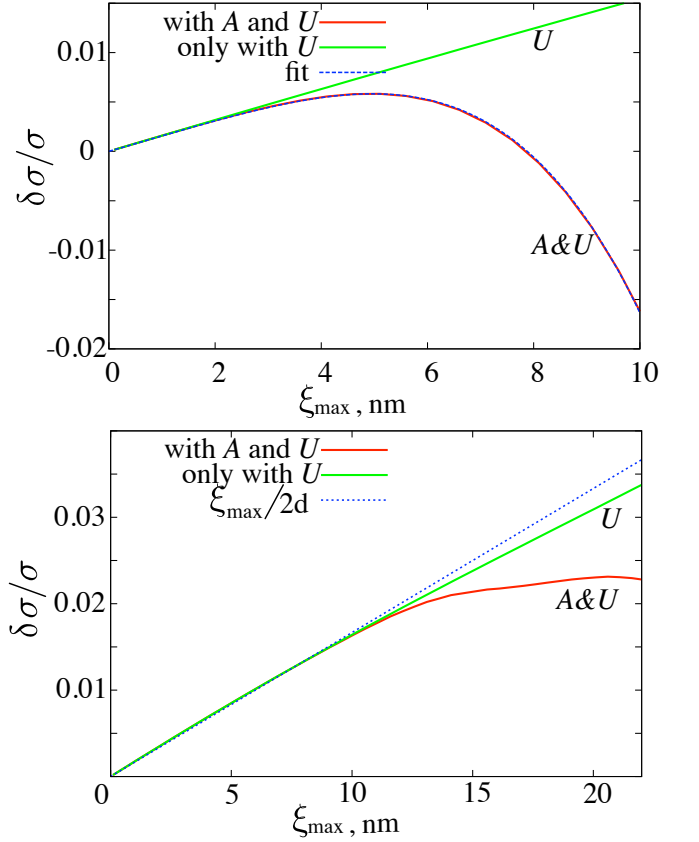


FIG. 8: Dependence of the piezocorrection to conductivity on the maximum deviation, $\delta\sigma(\xi_{max})/\sigma$, at the fixed gate voltage $V_g = 0.03$ V (top), 3 V (bottom). We show both the correction related to the term due to non-uniform pseudovector potential, and the contribution without this term. For $V_g = 0.03$ V, we also include the best fit $V = \alpha\xi_{max} + \beta\xi_{max}^4$ which represent the sum of linear in ξ_{max} correction due to charge redistribution and the correction due to nonuniform pseudovector potential $\beta\xi_{max}^4$. Parameters of the graphene flake are²⁶.

For high residual stress this correction is more important than due to charge redistribution, according to Ref. 17 it can block conductivity. For low residual stress it is about 10 times lower than the increasing conductivity correction. The oscillations of $\delta\sigma/\sigma$ have the period of $k_F L d$ are associated with the shift of Fabry-Perot resonances in conductivity for deformed graphene flake as compared with an undeformed flake. This shift occurs since the effective longitudinal wave vector of an electron in graphene depends on the deformation since it feels different charge density over the graphene flake. Note also that the contribution from pseudomagnetic fields does not oscillate since the value of k_F is the same for the whole flake. The first order perturbation theory in ξ_{max}/d is valid until this parameter reaches a rather large value, $\xi_{max}/d \sim 0.1$ (see Appendix for more details).

For the case of local deformation, using the graphene profile (2.23) and using the same technique as in Appendix, we find the correction for conductivity due to

the charge redistribution,

$$\frac{\delta\sigma}{\sigma} = \begin{cases} \xi_{max}/2d, & 1 \ll k_F L; \\ 0.088\xi_{max}(k_F L)^2/d, & k_F L \ll 1. \end{cases} \quad (3.14)$$

Note that the asymptotic behavior for large $k_F L$ has the same form as for homogeneous deformation.

We can also estimate the influence of inhomogeneous pseudomagnetic field assuming the local form of Hooke's law as in²⁴ and using the perturbation theory for the transfer matrix, as detailed in Appendix. We find that the first order perturbation theory correction in pseudovector potential vanishes, whereas the second order correction can be estimated as

$$\frac{\delta\sigma_A}{\sigma} \approx 5.5 \cdot 10^5 \frac{\xi_{max}^4}{L^4} \sqrt{\frac{d[\mu\text{m}]}{V_g[\text{V}]}}. \quad (3.15)$$

At low gate voltages and large deformations (for instance, induced by local deformation), this correction can be more important than the one from the charge redistribution, and thus the conductivity will be suppressed. From comparison of Eqs. (3.15) and (3.14) this suppression happens for deformations:

$$\frac{\xi_{max}}{L} > 10^{-2} \sqrt[6]{\frac{d[\mu\text{m}]}{V_g[\text{V}]}} \left(\frac{L}{d}\right)^{1/2}. \quad (3.16)$$

We demonstrate this by solving numerically by transfer matrix method the Dirac equation with additional potential due to charge redistribution and pseudovector potential, Fig. 7. At fixed large $\xi_{max} = 12$ nm (estimated using Eq. (3.16)) and at low voltages the conductivity starts to decrease due to inhomogeneous tension distribution in the flake, and at higher voltages increases again due to the effect of charge redistribution. Fig. 8 shows that for small gate voltages lower maximum deformation ξ_{max} is required to reach the point where the conductivity starts to decrease, in agreement with Eq. (3.15). For high gate voltages $V_g \sim 3$ V pseudomagnetic fields lead to saturation of the conductivity rather than to its decrease.

B. Two-gate geometry

Conductivity can also be used to measure relative stretching of deformed suspended graphene. Note that the influence of stretching on the conductivity of graphene deposited on a substrate has been demonstrated experimentally¹⁰. For suspended graphene it is more difficult to extract the value of stretching than from the graphene on the substrate, since the gate voltage simultaneously varies the concentration and deforms graphene, as shown above.

To measure relative stretching of suspended graphene, we propose the two-gate geometry (Fig. 9). The deformation of the graphene flake is created by the large bottom gate, the influence of the top gate on the deformation is

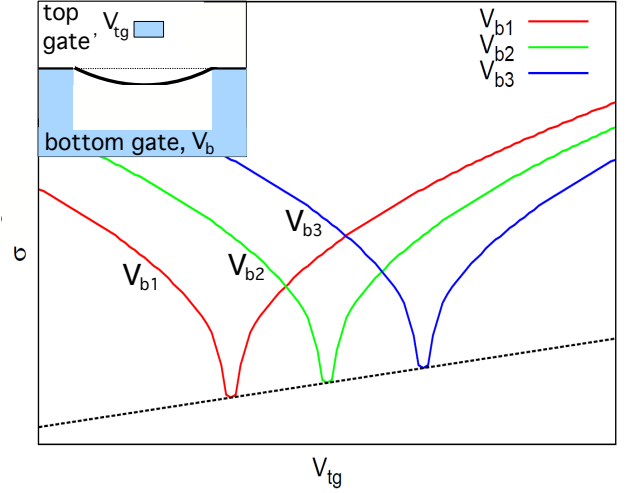


FIG. 9: Schematic dependence of conductivity of suspended graphene on the top gate voltage for several fixed bottom gate voltages. The conductivity at the Dirac point is slightly shifted due to change in Fermi velocity caused by deformation. The difference between the values of conductivity of the Dirac peaks for different bottom gate voltages, V_{b1} and V_{b2} , is proportional to the difference in relative deformations, $(\sigma_D(V_{b1}) - \sigma_D(V_{b2}))/\sigma_D \sim u_{xx}(V_{b1}) - u_{xx}(V_{b2})$.

small as the top gate is narrow. The top gate is used to vary the charge density in the region underneath it. In this geometry at the fixed voltage at the bottom gate one can move through the Dirac point by varying the voltage at the top gate (the experiment for bilayer with two gates on the substrate³⁴). The value of conductivity at this point depends on the deformation.

The stretching of the graphene flake, as discussed above, induces variations of the conductivity for two reasons. First, it induces pseudomagnetic fields. These, however, can be gauged away of Dirac equation³⁵ at the Dirac point and do not influence the conductivity. Second, it shifts the Fermi velocity. The relative shift is proportional to the deformation, $\delta v_F/v_F \sim \xi_{max}^2/L^2$, and leads to the positive correction of the conductivity at the Dirac point, $\delta\sigma/\sigma \sim \delta v_F/v_F \sim \xi_{max}^2/L^2$. Thus, for different bottom gate voltages, which is equivalent to different maximum deformations ξ_{max} , the conductivity at the Dirac point is slightly different, and the relative graphene stretching can be restored from this dependence. For example, consider the dependence of conductivity on the top gate voltage for different bottom gate voltages (Fig. 9). At a fixed value of the bottom gate voltage, the conductivity as a function of the top gate voltage exhibits a peak dependence, with the minimum corresponding to the Dirac point. The difference between the values of conductivity at Dirac peaks, σ_D , for different bottom gate voltages, V_{b1} and V_{b2} , is proportional to the difference in relative deformation, $(\sigma_D(V_{b1}) - \sigma_D(V_{b2}))/\sigma_D \sim u_{xx}(V_{b1}) - u_{xx}(V_{b2})$ (we remember that $u_{xx} \sim \xi_{max}^2/L^2$).

IV. DISCUSSION

In this Article, we investigated two mechanisms which affect the conductivity of suspended graphene — charge redistribution induced by the gate(s), and pseudomagnetic fields induced by the deformation of graphene. We find that for the small residual stress T_0 , the charge redistribution mechanism dominates. For low gate voltages and strong deformation, which experimentally is best realized by using AFM, the correction due to nonuniform pseudomagnetic fields is more significant. The correction due to pseudovector potential at the region of suspension can decrease conductivity at the large residual stress¹⁷. It is important that the two mechanisms provide corrections to conductivity which are of different signs. Indeed, the correction from pseudomagnetic fields suppresses the conductivity¹⁷ by shifting K-points due to the vector potential. The shift is different at different points of the suspended sample, and if the deformation is big enough, the Fermi circles at the clamping points and at the centre of the flake do not overlap: The system becomes insulating. If now we take into account the effects of the gate, not only the Fermi circles are shifted, but their radii are greater at the center of the flake since the charge density is greater in the areas closer to the gate. The increase of the radii and the shift of the center compete, and we find that typically the radius increase is more important.

It is difficult to measure piezoconductivity only by using a bottom gate since the gate voltage not only bends graphene and produces the correction to the conductivity, but also shifts the overall charge density. The density dependence of the conductivity is different from the density dependence of the correction. Thus, to extract the value of piezoconductivity, one has to compare the conductance of deformed and undeformed graphene sheet at the same density, which can only be done in the one-gate geometry by comparing the results with the theoretical prediction. In contrast, the two-gate setup, with a bottom gate fixing the overall density and the top gate (which can be an AFM tip) creating the deformation is more convenient to extract piezoconductivity. One can fix the voltage on the bottom gate and start to deform the flake with the AFM tip. At low gate voltages the conductivity decreases due to the pseudomagnetic fields, whereas at higher voltages it starts to grow due to the charge redistribution.

In the real experimental situation, the AFM tip has a point shape, whereas in this Article we considered for illustration the deformation homogeneous in one direction, *i.e.* replaced the tip by a rod. Non-homogeneous deformation in all directions creates pseudomagnetic fields, with the conductivity depending not only on the transverse displacement, but also locally on the position over the graphene sheet. The conductivity is the largest if the tip is placed in the middle of the sheet, and decreases if the tip moves to the side. We can understand this behavior from a simple reasoning. Indeed, the electrons which from the two sides of the tip feel the pseudomagnetic

fields and interfere similarly to an Aharonov-Bohm ring. The interference is more destructive if the tip is further from the center, and thus the conductivity decreases.

Another parameter which affects the conductivity is the residual stress T_0 . It can be varied experimentally for instance if one uses graphene suspended over piezoelectric substrate. Putting voltage on the substrate would induce extra stress on graphene, and one can move from the situation where pseudovector potential blocks the conductivity at low gate voltages to the case where residual stress does not play a role and the correction due to charge redistribution increases the conductivity.

In this Article, we considered ideal ballistic graphene. In particular, we disregarded the contact resistance, assuming the clamping points to be ideal contacts. Finite transparency of the contacts would suppress both the conductivity itself and the piezocorrection to the conductivity; in addition, it would raise the amplitude of Fabry-Perot resonances.

For strong deformations of the graphene sheet, the problem becomes much more complicated, since one has now to solve elasticity equations self-consistently, taking into account that the displacement depends on the charge redistribution. This leads to additional terms in the equations of the elasticity theory. Taking into account influence of the density redistribution on the term with electrostatic pressure in the equation of deformation, one can show that the self-consistency condition increases the deformation in the middle of the graphene sheet. This effect only becomes important at sufficiently strong deformations.

Finally, we assumed that undeformed graphene is flat. In reality, it is always rippled, and, in principle, one needs to use the elasticity theory for membranes. However, we do not expect that taking ripples into account would significantly affect the results of this paper. First, the ripples are small and have a large radius of curvature, which means they are very little affected by the overall deformation of the graphene sheet. Second, the main effect of the ripples is to renormalize the energy over the graphene sheet³⁶. We thus expect that our results are valid, but for renormalized energy over the flake (energy is determined by gate voltage in clean case, and is renormalized in the rippled case).

V. ACKNOWLEDGEMENTS

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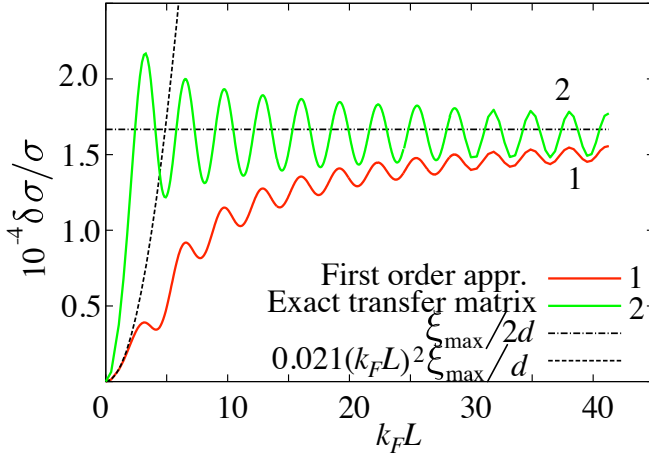


FIG. 10: Dependence of the relative correction to conductivity on $k_F L$, $\delta\sigma/\sigma(k_F L)$ for constant $\xi_{\max}/d = 1/3000$, for the correction of the first order in ξ_{\max}/d , Eq. (6.6), the curve 1, and exact transfer matrix solution of integral equation, the curve 2. The correction from the exact solution has the same dependence on $k_F L$ as the first order correction, the oscillations are in the same phase. Asymptotics for small and large $k_F L$, Eq. (3.10), are shown as dashed lines. Parameters of the flake are²⁶.

VI. APPENDIX. PERTURBATIVE CORRECTIONS TO CONDUCTIVITY

In this Appendix, we calculate the corrections to the conductivity due to both charge redistribution and pseudomagnetic fields, using the perturbation theory.

The Dirac equation for one valley in graphene has the form

$$v_F \vec{\sigma} \vec{p} + \delta U(x, y) = E, \quad (6.1)$$

with $\vec{\sigma} = (\sigma_x, \sigma_y)$, $\vec{p} = (p_x, p_y)$,

$$p_x = -i\hbar\partial_x + A_x, p_y = -i\hbar\partial_y + A_y,$$

$A_x(x, y)$ and $A_y(x, y)$ being the components of the pseudomagnetic vector-potential³⁰, given by Eq. (3.2), and $\delta U(x, y)$ is the additional electrostatic potential due to the charge redistribution over the graphene flake. It is determined by local variations of the Fermi energy over the flake. Since the Fermi energy depends on the charge density over the flake, $E_F(x) = \hbar v_F k_F(x)$, $k_F(x) = \sqrt{\pi n(x)/e}$, one has

$$\delta U(x)/E = \delta k_F(x)/k_F = \delta n(x)/2n = \xi(x)/2d.$$

We only consider the deformation homogeneous in y -direction. Then both A_y and δU only depend on the coordinate x , and $A_x = 0$ (see Section III). The problem becomes effectively one-dimensional since the momentum q in y -direction is conserved. It is convenient to use the transfer matrix representation of Dirac equation³⁶ to calculate the correction to the conductivity caused by the

deformation $A_y(x)$, $\delta U(x)$,

$$\begin{aligned} \mathcal{T}_H(x_2, x_1) &= \mathcal{T}_{0H}(x_2, x_1) - \\ &- \int_{x_1}^{x_2} dx \mathcal{T}_{0H}(x_2, x) (\sigma_z \delta U(x) + i\sigma_x A_y(x)) \mathcal{T}_H(x, x_1), \end{aligned} \quad (6.2)$$

where \mathcal{T}_H is the Hadamard transformed transfer matrix, and \mathcal{T}_{0H} is the Hadamard transformed transfer matrix of the unperturbed system,

$$\mathcal{T}_{0H} = \exp(i\sigma_z k_F L + \sigma_x q L). \quad (6.3)$$

We perform the perturbation expansion of the integral form for Eq. (6.3), and in the first order in $\delta U(x)$ and $A_y(x)$ we obtain

$$\begin{aligned} \mathcal{T}_1(x_2, x_1) &= \mathcal{T}_0(x_2, x_1) - \\ &- i \int_{x_1}^{x_2} dx \mathcal{T}_0(x_2, x) (\sigma_z \delta U(x) + i\sigma_x A_y(x)) \mathcal{T}_0(x, x_1). \end{aligned} \quad (6.4)$$

The conductance of the graphene sheet is determined by Landauer formula (3.1). According to general scattering theory³⁶, the transmission matrix element \hat{t} is an inverse element of \mathcal{T}_H ,

$$\hat{t} = (\mathcal{T}_H^{-})^{-1}. \quad (6.5)$$

Taking into account Eq. (6.5), Landauer formula (3.1), and the definition (6.5), the first order corrections to conductivity due to electrostatics and pseudo-magnetic field are

$$\delta\sigma_U = \sum_q 4|t_q|^4 I_U k_F L \frac{q^2 k_F}{k^3} \sin kL, \quad (6.6)$$

$$I_U = \int_0^L \frac{dx}{L} \frac{\xi(x)}{2d} \sin k(L-x) \sin kx,$$

$$\delta\sigma_A = \sum_q 2|t_q|^4 \frac{k_F q}{k^2} I_A, \quad (6.7)$$

$$\begin{aligned} I_A &= \int_0^L dx \delta A(x) \times \\ &\times (\sin^2 kL - 2 \cos kL \sin kx \sin k(L-x)), \end{aligned} \quad (6.8)$$

where $q = 2\pi n/W$ is a wave vector in the y -direction, n is an integer number, and k is a wave vector along the strip,

$$k^2 + q^2 = k_F^2.$$

Furthermore, t_q is the transmission probability for clean system for the mode q , and

$$|t_q|^2 = (\cos^2 kL + k_F^2 \sin^2 kL/k^2)^{-1}.$$

Note that the first-order correction due to the pseudo-vector potential (6.7) only contains odd powers of q , so that the sum over q vanishes. Thus, the first-order correction to the conductivity is determined solely by the

density redistribution. It is linear in the maximum deviation ξ_{max}/d for small deviations.

First, we remark on the validity of Eq. (6.6). The expansion of the expression

$$1 - 4(t_q t_q^\dagger)^2 I_U k_F L \frac{q^2 k_F}{k^3} \sin kL$$

has been made under assumption that the second term is small in comparison with unity due to the small prefactor $\xi_{max} k_F L/d$. Following this argument, the expression for the first order correction to the conductivity in ξ_{max}/d is formally only valid for $\xi_{max}/dk_F L \ll 1$. However, solving the integral equation numerically, we find that this expression is valid for a broader parameter range. We compare results of calculations for the first order correction Eq. (6.6) and numerical solution of Eq. (6.3) for the two cases: for the fixed ratio ξ_{max}/d and for the fixed value of $k_F L$. For the first case, the dependence of $\delta\sigma/\sigma$ on $k_F L$ shows the same oscillation period and the same asymptotic behavior at large $k_F L$, Fig. 10. For the second case, at large $k_F L \sim 40$ (for the distance to the gate $d = 300$ nm this corresponds to the gate voltage $V_g = 3$ V) the expansion clearly ceases to be valid, see Fig. 11. We thus conclude from the results of our numerical solution that the expression for the correction linear in ξ_{max}/d is applicable until $\xi_{max}/d \ll 1$, which is weaker than the perturbation theory suggestion $\xi_{max} k_F L/d \ll 1$.

The second order correction to conductivity contains also a term with the pseudo-vector potential, the magnitude of the term being $(\xi_{max}/L)^4$.

We consider both corrections separately. Now we perform the analysis of Eq. (6.6) for deformation with constant pressure. For this case, the shape of the strip is nearly parabolic (Section II) and can be approximated as

$$\xi(x) = \frac{4\xi_{max}}{L^2}(x - L/2)^2.$$

The integral with the induced potential $\delta U(x)$ from Eq. (6.6), I_U , is

$$I_U = \frac{\xi_{max}}{12d} \frac{kL(6 - (kL)^2) \cos kL - 3(2 - (kL)^2) \sin kL}{(kL)^3}. \quad (6.9)$$

Now we can perform the summation over modes for $\delta\sigma$, Eq. (6.6), analytically in two asymptotic cases: $k_F L \ll 1$ and $k_F L \gg 1$.

For $k_F L \ll 1$, the evanescent modes give the most important contribution to the conductivity¹,

$$\sigma(k_F L \ll 1) = \frac{W}{2\pi L} \int_{-\infty}^{\infty} \frac{dx}{\cosh^2 x} = \frac{W}{\pi L}, \quad (6.10)$$

and to the correction to the conductivity,

$$\delta\sigma(k_F L \ll 1) = \frac{\xi_{max}}{3d} \frac{W}{2\pi L} (k_F L)^2 I, \quad (6.11)$$

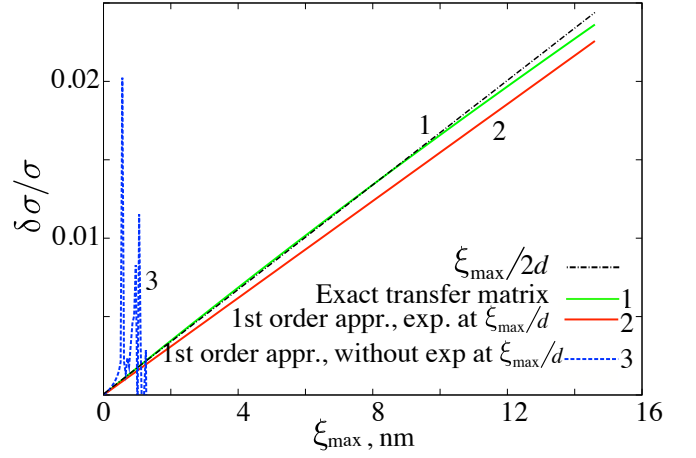


FIG. 11: Dependence of the relative correction to conductivity on the maximum deformation, $\delta\sigma(\xi_{max})/\sigma$ for constant $k_F L = 40$, in the first order in ξ_{max}/d , Eq. (6.6), the curve 2, and the exact transfer matrix solution of integral equation, the curve 2. Both the expansion and summation of the $(\mathcal{T}^{--})^{-1}$ are not valid for $\xi_{max} k_F L/d > 1$ for small parameter as mentioned in the text. The dashed line, the curve 3, is the summation result. The exact solution shows linear dependence on deviation even for rather large deviation, and this linear dependence is close both to the correction Eq. (6.6) and to the correction averaged over fast oscillations, $\xi_{max}/2d$. Parameters of the flake are²⁶.

with

$$I = 2 \int_0^\infty \frac{dx \sinh x (x(6 + x^2) \cosh x - 3(2 + x^2) \sinh x)}{x^4 \cosh^4 x},$$

and its numerical value is $I \approx 0.124$. The relative correction to conductivity reads

$$\frac{\delta\sigma}{\sigma} = \frac{\xi_{max} I}{6d} (k_F L)^2 \approx 0.021 \frac{\xi_{max}}{d} (k_F L)^2. \quad (6.12)$$

For $k_F L \gg 1$ we average over fast oscillations. In this case, only the propagating modes contribute significantly to the conductivity.

To perform the averaging, we replace the summation over q by the integration,

$$\sum_q \rightarrow \frac{W}{2\pi} \int dq.$$

To simplify subsequent calculations, we make the change of variables $q = k_F \sin \phi$, $k = k_F \cos \phi$, and then go from the integral over dq to the integral over $d\phi$. The correction to the conductivity Eq. (6.6) has the form

$$\delta\sigma = \frac{k_F W}{\pi} \frac{\xi_{max}}{d} \times \int_0^{\pi/2} d\phi \frac{\cos \phi \sin^2 \phi \sin^2(k_F L \cos \phi)}{(\cos^2 \phi \cos^2(k_F L \cos \phi) + \sin^2(k_F L \cos \phi))^2}.$$

In this expression only the term with $3 \sin kL/kL$ from Eq.(6.9) survived: All terms with $\cos kL$ vanish

after averaging, and the term with $-6 \sin kL/(kL)^3$ is smaller than one which is taken into account). For large k_FL the terms $\cos(k_FL \cos \phi)$ and $\sin(k_FL \sin \phi)$ in Eq. (6.6) oscillate very rapidly. We can represent $\int_0^{\pi/2} d\phi$ as a sum of fast oscillating terms, with each term being an average over the period,

$$\int_0^{\pi/2} d\phi \longrightarrow \sum_{n=0}^{N_{max}} \int_{\phi_n}^{\phi_{n+1}} d\phi f(\phi_{n+1/2}, \cos(k_FL \cos \phi), \sin(k_FL \sin \phi)),$$

with $k_FL \sin \phi_n = 2\pi n$. The integrand f is determined by structure of Eq. (6.6) and Eq. (6.9),

$$\int_0^{2\pi} f(\phi) = \int_0^{2\pi} \frac{\sin^2 x dx}{(a^2 \cos^2 x + \sin^2 x)^2} = \frac{2\pi}{a}.$$

What is left is the sum over n ,

$$\delta\sigma = \frac{\xi_{max}}{d} \frac{k_FW}{\pi} 2\pi \sum_n \sqrt{1 - (x_n/k_FL)^2}, \quad (6.13)$$

$x_n = \pi(2n + 1)$. Finally,

$$\delta\sigma = \frac{\xi_{max}}{8d} k_FW. \quad (6.14)$$

The conductivity after averaging over fast oscillations becomes $\sigma = k_FW/4$, and the relative correction to the conductivity is

$$\frac{\delta\sigma}{\sigma} = \frac{\xi_{max}}{2d}.$$

From general physical considerations about the correction (see main text), one also expects the dependence $\delta\sigma/\sigma \sim \xi_{max}/d$ for $\delta\sigma/\sigma$.

Concerning the correction due to the pseudomagnetic fields, it is of the second order in δA , and the analytical expressions are too cumbersome. Instead, we illustrate our conclusions using the numerical solution of the integral equation (6.3). It is done by multiplying transfer matrices for small intervals of the length δx . Convergence with the size of δx is reached.

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